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STANDARDIZED

UXO TECHNOLOGY DEMONSTRATION SITE

OPEN FIELD SCORING RECORD NO. 740

SITE LOCATION: U.S. ARMY ABERDEEN PROVING GROUND

> DEMONSTRATOR: GEOPHEX, LTD. 605 MERCURY STREET RALEIGH, NC 27603-2343

TECHNOLOGY TYPE/PLATFORM: GEM-5/TOWED ARRAY

PREPARED BY:
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ABERDEEN PROVING GROUND, MD 21005-5059

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SECTION 1. GENERAL INFORMATION

1.1 BACKGROUND

Technologies under development for the detection and discrimination of munitions and explosives of concern (MEC) – i.e. unexploded ordnance (UXO) and discarded military munitions (DMM) require testing so that their performance can be characterized. To that end, Standardized Test Sites have been developed at Aberdeen Proving Ground (APG), Maryland and U.S. Army Yuma Proving Ground (YPG), Arizona. These test sites provide a diversity of geology, climate, terrain, and weather as well as diversity in ordnance and clutter. Testing at these sites is independently administered and analyzed by the government for the purposes of characterizing technologies, tracking performance with system development, comparing performance of different systems, and comparing performance in different environments.

The Standardized UXO Technology Demonstration Site Program is a multi-agency program spearheaded by the U.S. Army Environmental Center (AEC). The U.S. Army Aberdeen Test Center (ATC) and the U.S. Army Corps of Engineers Engineering Research and Development Center (ERDC) provide programmatic support. The program is being funded and supported by the Environmental Security Technology Certification Program (ESTCP), the Strategic Environmental Research and Development Program (SERDP) and the Army Environmental Quality Technology Program (EQT).

1.2 SCORING OBJECTIVES

The objective in the Standardized UXO Technology Demonstration Site Program is to evaluate the detection and discrimination capabilities of a given technology under various field and soil conditions. Inert munitions and clutter items are positioned in various orientations and depths in the ground.

The evaluation objectives are as follows:

- a. To determine detection and discrimination effectiveness under realistic scenarios that vary targets, geology, clutter, topography, and vegetation.
 - b. To determine cost, time, and manpower requirements to operate the technology.
- c. To determine demonstrator's ability to analyze survey data in a timely manner and provide prioritized "Target Lists" with associated confidence levels.
- d. To provide independent site management to enable the collection of high quality, ground-truth, geo-referenced data for post-demonstration analysis.

1.2.1 Scoring Methodology

a. The scoring of the demonstrator's performance is conducted in two stages. These two stages are termed the RESPONSE STAGE and DISCRIMINATION STAGE. For both stages, the probability of detection (P_d) and the false alarms are reported as receiver-operating

characteristic (ROC) curves. False alarms are divided into those anomalies that correspond to emplaced clutter items, measuring the probability of false positive (P_{fp}), and those that do not correspond to any known item, termed background alarms.

- b. The RESPONSE STAGE scoring evaluates the ability of the system to detect emplaced targets without regard to ability to discriminate ordnance from other anomalies. For the blind grid RESPONSE STAGE, the demonstrator provides the scoring committee with a target response from each and every grid square along with a noise level below which target responses are deemed insufficient to warrant further investigation. This list is generated with minimal processing and, since a value is provided for every grid square, will include signals both above and below the system noise level.
- c. The DISCRIMINATION STAGE evaluates the demonstrator's ability to correctly identify ordnance as such and to reject clutter. For the blind grid DISCRIMINATION STAGE, the demonstrator provides the scoring committee with the output of the algorithms applied in the discrimination-stage processing for each grid square. The values in this list are prioritized based on the demonstrator's determination that a grid square is likely to contain ordnance. Thus, higher output values are indicative of higher confidence that an ordnance item is present at the specified location. For digital signal processing, priority ranking is based on algorithm output. For other discrimination approaches, priority ranking is based on human (subjective) judgment. The demonstrator also specifies the threshold in the prioritized ranking that provides optimum performance, (i.e. that is expected to retain all detected ordnance and rejects the maximum amount of clutter).
- d. The demonstrator is also scored on EFFICIENCY and REJECTION RATIO, which measures the effectiveness of the discrimination stage processing. The goal of discrimination is to retain the greatest number of ordnance detections from the anomaly list, while rejecting the maximum number of anomalies arising from non-ordnance items. EFFICIENCY measures the fraction of detected ordnance retained after discrimination, while the REJECTION RATIO measures the fraction of false alarms rejected. Both measures are defined relative to performance at the demonstrator-supplied level below which all responses are considered noise, i.e., the maximum ordnance detectable by the sensor and its accompanying false positive rate or background alarm rate.
- e. Based on configuration of the ground truth at the standardized sites and the defined scoring methodology, there exists the possibility of having anomalies within overlapping halos and/or multiple anomalies within halos. In these cases, the following scoring logic is implemented:
- (1) In situations where multiple anomalies exist within a single R_{halo} , the anomaly with the strongest response or highest ranking will be assigned to that particular ground truth item.
- (2) For overlapping R_{halo} situations, ordnance has precedence over clutter. The anomaly with the strongest response or highest ranking that is closest to the center of a particular ground truth item gets assigned to that item. Remaining anomalies are retained until all matching is complete.

- (3) Anomalies located within any R_{halo} that do not get associated with a particular ground truth item are thrown out and are not considered in the analysis.
- f. All scoring factors are generated utilizing the Standardized UXO Probability and Plot Program, version 3.1.1.

1.2.2 Scoring Factors

Factors to be measured and evaluated as part of this demonstration include:

- a. Response Stage ROC curves:
- (1) Probability of Detection (P_d^{res}).
- (2) Probability of False Positive (P_{fp}^{res}).
- (3) Background Alarm Rate (BAR^{res}) or Probability of Background Alarm (P_{BA}^{res}).
- b. Discrimination Stage ROC curves:
- (1) Probability of Detection (P_d^{disc}) .
- (2) Probability of False Positive (P_{fo}^{disc}).
- (3) Background Alarm Rate (BAR^{disc}) or Probability of Background Alarm (P_{BA}^{disc}).
- c. Metrics:
- (1) Efficiency (E).
- (2) False Positive Rejection Rate (R_{fp}).
- (3) Background Alarm Rejection Rate (R_{BA}).
- d. Other:
- (1) Probability of Detection by Size and Depth.
- (2) Classification by type (i.e., 20-, 40-, 105-mm, etc.).
- (3) Location accuracy.
- (4) Equipment setup, calibration time and corresponding man-hour requirements.
- (5) Survey time and corresponding man-hour requirements.

- (6) Reacquisition/resurvey time and man-hour requirements (if any).
- (7) Downtime due to system malfunctions and maintenance requirements.

1.3 STANDARD AND NONSTANDARD INERT ORDNANCE TARGETS

The standard and nonstandard ordnance items emplaced in the test areas are listed in Table 1. Standardized targets are members of a set of specific ordnance items that have identical properties to all other items in the set (caliber, configuration, size, weight, aspect ratio, material, filler, magnetic remanence, and nomenclature). Nonstandard targets are inert ordnance items having properties that differ from those in the set of standardized targets.

TABLE 1. INERT ORDNANCE TARGETS

Standard Type	Nonstandard (NS)	
20-mm Projectile M55	20-mm Projectile M55	
	20-mm Projectile M97	
40-mm Grenades M385	40-mm Grenades M385	
40-mm Projectile MKII Bodies	40-mm Projectile M813	
BDU-28 Submunition		
BLU-26 Submunition		
M42 Submunition		
57-mm Projectile APC M86		
60-mm Mortar M49A3	60-mm Mortar (JPG)	
	60-mm Mortar M49	
2.75-inch Rocket M230	2.75-inch Rocket M230	
	2.75-inch Rocket XM229	
MK 118 ROCKEYE		
81-mm Mortar M374	81-mm Mortar (JPG)	
	81-mm Mortar M374	
105-mm Heat Rounds M456		
105-mm Projectile M60	105-mm Projectile M60	
155-mm Projectile M483A1	155-mm Projectile M483A	
	500-lb Bomb	

JPG = Jefferson Proving Ground HEAT = high-explosive antitank

SECTION 2. DEMONSTRATION

2.1 DEMONSTRATOR INFORMATION

2.1.1 Demonstrator Point of Contact (POC) and Address

POC: Mr. Bill SanFilipo

(919) 839-8515

Address: Geophex, Ltd.

605 Mercury Street

Raleigh, NC 27603-2343

2.1.2 System Description (provided by demonstrator)

The GEM-5 array sensor consists of a single large rectangular transmitting coil (Tx) and seven receiver coil (Rx) coaxial pairs (fig. 1) wired in a differential (gradient) mode, an electronic console incorporating seven analog-to-digital converters (ADCs) and digital signal processors (DSPs) and a digitally controlled Tx current driver, and a laptop personal computer data logger. Data time stamping is performed with a real-time clock for synchronization to a Differential Global Positioning System (DGPS), and two DGPS units provide positioning for the seven receivers and the operator navigation computer. The conceptual representation of the GEM-5 array with single Tx (red) and symmetric positioning of Rx differencing coil pairs to null the primary field (the system for this demonstration has seven Rx pairs; the red Q-coil represents a target) is shown in Figure 2.

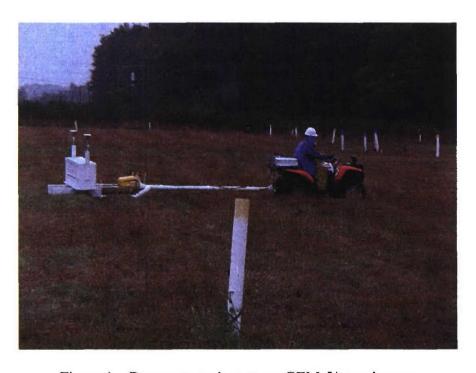


Figure 1. Demonstrator's system, GEM-5/towed array.

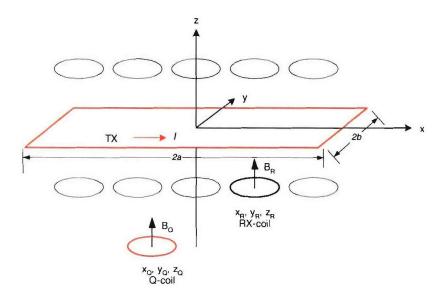


Figure 2. Demonstrator's system, GEM-5/towed array

The system is a continuous-wave frequency-domain electromagnetic interference (EMI) sensor that uses a hybrid current waveform to provide simultaneous multifrequency (typically 10 log-spaced) energy in the 90-Hz to 90-kHz band, with each Rx DSP performing digital Fourier transforms at the selected frequencies. The upper Rx coil provides primary field reference (amplitude and phase) for Rx output normalization (units of parts per million (ppm) of the primary field generated electromagnetic field (EMF).

2.1.3 Data Processing Description (provided by demonstrator)

Target detection is achieved by combining multifrequency data into a single detection channel designed to respond particularly to metal targets and not to geologic anomalies. Data collected include the sum of all quadrature channels, the difference between high-frequency and low-frequency inphase channels, the sum of the absolute differences of quadrature channels between all frequency pairs, and the inverse log (frequency) weighted total apparent conductivity. The selected detection channel forms the response stage. The DGPS georeferenced detection channel data are processed with an automatic anomaly picker that identifies target anomalies above a specified threshold, excluding single-point anomalies and overlapping secondary anomalies.

Georeferencing uses the time stamps to interpolate 15- or 30-Hz GEM-5 position between 1-Hz DGPS fixes and the position for each sensor from spatial interpolation between two DGPS antennas. The raw DGPS lat/lon fixes are transformed to Universal Transverse Mercator (UTM) during the post-processing.

Target identification and classification (clutter discrimination) use a normalized matching of the multifrequency spectra to a library of known UXO spectral responses. The matching scheme fits an unknown target to the best-fit linear combination of the longitudinal (sensor axis

axis) response spectra, allowing for a frequency independent background inphase response for magnetic soils. The goodness-of-fit to the best-fitting item is mapped into a confidence ranking from 0 (definite clutter) to 10 (definite UXO) with 5 corresponding to the clutter misfit threshold. The confidence ranking forms the discrimination stage.

2.1.4 Data Submission Format

Data were submitted for scoring in accordance with data submission protocols outlined in the Standardized UXO Technology Demonstration Site Handbook. These submitted data are not included in this report in order to protect ground truth information.

2.1.5 <u>Demonstrator Quality Assurance (QA) and Quality Control (QC) (provided by demonstrator)</u>

QC: Daily sensor calibration check with ferrite target within the calibration area test.

QA: Daily review of data.

2.1.6 Additional Records

The following record(s) by this vendor can be accessed via the Internet as MicroSoft Word documents at www.uxotestsites.org. The blind grid counterpart to this report is Scoring Record No. 739.

2.2 APG SITE INFORMATION

2.2.1 Location

The APG Standardized Test Site is located within a secured range area of the Aberdeen Area. The Aberdeen Area of APG is located approximately 30 miles northeast of Baltimore at the northern end of the Chesapeake Bay. The Standardized Test Site encompasses 17 acres of upland and lowland flats, woods and wetlands.

2.2.2 Soil Type

According to the soils survey conducted for the entire area of APG in 1998, the test site consists primarily of Elkton Series type soil (ref 2). The Elkton Series consist of very deep, slowly permeable, poorly drained soils. These soils formed in silty aeolin sediments and the underlying loamy alluvial and marine sediments. They are on upland and lowland flats and in depressions of the Mid-Atlantic Coastal Plain. Slopes range from 0 to 2 percent.

ERDC conducted a site-specific analysis in May of 2002 (ref 3). The results basically matched the soil survey mentioned above. Seventy percent of the samples taken were classified as silty loam. The majority (77 percent) of the soil samples had a measured water content between 15- and 30-percent with the water content decreasing slightly with depth.

For more details concerning the soil properties at the APG test site, go to www.uxotestsites.org on the web to view the entire soils description report.

2.2.3 Test Areas

A description of the test site areas at APG is included in Table 2.

TABLE 2. TEST SITE AREAS

Area	Description				
Calibration Grid	Contains 14 standard ordnance items buried in six positions at various angles and depths to allow demonstrator to calibrate their equipment.				
Blind Test Grid	Contains 400 grid cells in a 0.2-hectare (0.5 acre) site. The center of each grid cell contains ordnance, clutter or nothing.				
Open Field	A 4-hectare (10-acre) site containing open areas, dips, ruts and obstructions that challenge platform systems or hand held detectors. The challenges include a gravel road, wet areas and trees. The vegetation height varies from 15 to 25 cm.				

SECTION 3. FIELD DATA

3.1 DATE OF FIELD ACTIVITIES (7 and 17 through 20 October 2005)

3.2 AREAS TESTED/NUMBER OF HOURS

Areas tested and total number of hours operated at each site are summarized in Table 3.

TABLE 3. AREAS TESTED AND NUMBER OF HOURS

Area	Number of Hours
Calibration Lanes	1.16
Open Field	47.50

3.3 TEST CONDITIONS

3.3.1 Weather Conditions

An APG weather station located approximately one mile west of the test site was used to record average temperature and precipitation on a half hour basis for each day of operation. The temperatures listed in Table 4 represent the average temperature during field operations from 0700 to 1700 hours while precipitation data represents a daily total amount of rainfall. Hourly weather logs used to generate this summary are provided in Appendix B.

TABLE 4. TEMPERATURE/PRECIPITATION DATA SUMMARY

Date, 2005	Average Temperature, °F	Total Daily Precipitation, in.
07 October	75.1	1.21
17 October	59.2	0.00
18 October	67.1	0.00
19 October	61.7	0.00
20 October	55.1	0.00

3.3.2 Field Conditions

Geophex surveyed the open field 7 and 17 through 20 October. Other than a couple small wet spots, the field was dry and in optimal condition throughout their survey.

3.3.3 Soil Moisture

Three soil probes were placed at various locations within the site to capture soil moisture data: blind grid, calibration lanes, mogul, and wooded areas. Measurements were collected in percent moisture and were taken twice daily (morning and afternoon) from five different soil depths (1 to 6 in., 6 to 12 in., 12 to 24 in., 24 to 36 in., and 36 to 48 in.) from each probe. Soil moisture logs are included in Appendix C.

3.4 FIELD ACTIVITIES

3.4.1 Setup/Mobilization

These activities included initial mobilization and daily equipment preparation and breakdown. A two-person crew took 13 hours and 30 minutes to perform the initial setup and mobilization. There was 4 hours and 10 minutes of daily equipment preparation and end of the day equipment breakdown lasted 3 hours and 50 minutes.

3.4.2 Calibration

Geophex spent a total of 1 hour and 10 minutes in the calibration lanes, of which 35 minutes was spent collecting data.

3.4.3 Downtime Occasions

Occasions of downtime are grouped into five categories: equipment/data checks or equipment maintenance, equipment failure and repair, weather, Demonstration Site issues, or breaks/lunch. All downtime is included for the purposes of calculating labor costs (section 5) except for downtime due to Demonstration Site issues. Demonstration Site issues, while noted in the Daily Log, are considered non-chargeable downtime for the purposes of calculating labor costs and are not discussed. Breaks and lunches are discussed in this section and billed to the total Site Survey area.

- **3.4.3.1** Equipment/data checks, maintenance. Equipment data checks and maintenance activities accounted for 15 minutes of site usage time. These activities included changing out batteries and routine data checks to ensure the data was being properly recorded/collected. Geophex spent an additional 55 minutes for breaks and lunches.
- **3.4.3.2** Equipment failure or repair. A total of 11 hours and 25 minutes was needed to resolve equipment failures that occurred while surveying the open field. Geophex had separate four issues of their PVC sled breaking. Each time Geophex fixed the sled by gluing and installing new PVC material.
- **3.4.3.3** Weather. No weather delays occurred during the survey.

3.4.4 Data Collection

Geophex spent a total time of 47 hours and 30 minutes in the open field area, 26 hours and 55 minutes of which was spent collecting data.

3.4.5 Demobilization

The Geophex survey crew went on to conduct a full demonstration of the site. Therefore, demobilization did not occur until 21 October 2005. On that day, it took the crew 2 hours and 5 minutes to break down and pack up their equipment.

3.5 PROCESSING TIME

Geophex submitted the raw data from the demonstration activities on the last day of the demonstration, as required. The scoring submittal data was provided 30 November 2005.

3.6 DEMONSTRATOR'S FIELD PERSONNEL

Mr. Bill SanFilipo Mr. Karlin Yupichak

3.7 DEMONSTRATOR'S FIELD SURVEYING METHOD

Geophex surveyed the open field in a circular fashion. The team then filled in the rest of the open field by sections in a linear manner.

3.8 SUMMARY OF DAILY LOGS

Daily logs capture all field activities during this demonstration and are located in Appendix D. Activities pertinent to this specific demonstration are indicated in highlighted text.

SECTION 4. TECHNICAL PERFORMANCE RESULTS

4.1 ROC CURVES USING ALL ORDNANCE CATEGORIES

Figure 2 shows the probability of detection for the response stage (P_d^{res}) and the discrimination stage (P_d^{disc}) versus their respective probability of false positive. Figure 3 shows both probabilities plotted against their respective background alarm rate. Both figures use horizontal lines to illustrate the performance of the demonstrator at two demonstrator-specified points: at the system noise level for the response stage, representing the point below which targets are not considered detectable, and at the demonstrator's recommended threshold level for the discrimination stage, defining the subset of targets the demonstrator would recommend digging based on discrimination. Note that all points have been rounded to protect the ground truth.

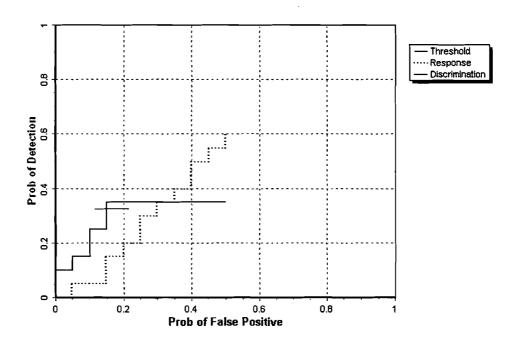


Figure 2. GEM-5/towed array open field probability of detection for response and discrimination stages versus their respective probability of false positive over all ordnance categories combined.

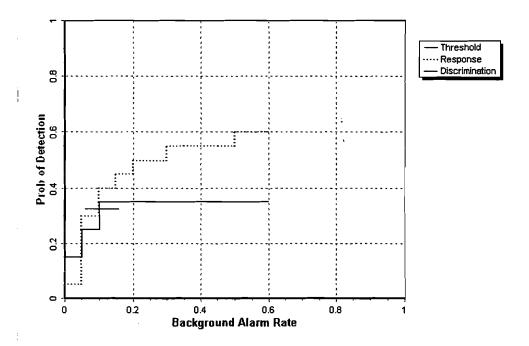


Figure 3. GEM-5/towed array open field probability of detection for response and discrimination stages versus their respective background alarm rate over all ordnance categories combined.

4.2 ROC CURVES USING ORDNANCE LARGER THAN 20 MM

Figure 4 shows the probability of detection for the response stage (P_d^{res}) and the discrimination stage (P_d^{disc}) versus their respective probability of false positive when only targets larger than 20 mm are scored. Figure 5 shows both probabilities plotted against their respective background alarm rate. Both figures use horizontal lines to illustrate the performance of the demonstrator at two demonstrator-specified points: at the system noise level for the response stage, representing the point below which targets are not considered detectable, and at the demonstrator's recommended threshold level for the discrimination stage, defining the subset of targets the demonstrator would recommend digging based on discrimination. Note that all points have been rounded to protect the ground truth.

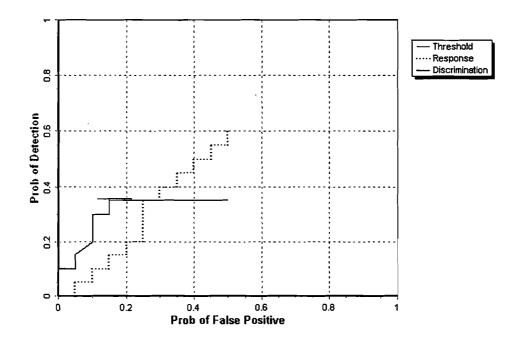


Figure 4. GEM-5/towed array open field probability of detection for response and discrimination stages versus their respective probability of false positive for all ordnance larger than 20 mm.

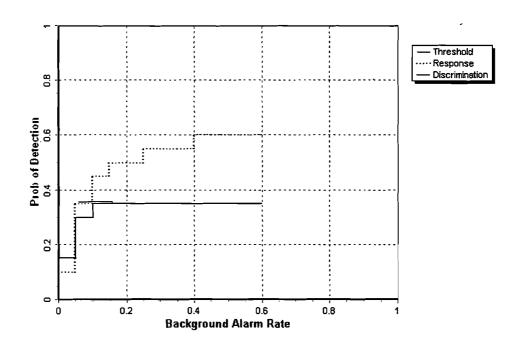


Figure 5. GEM-5/towed array open field probability of detection for response and discrimination stages versus their respective background alarm rate for all ordnance larger than 20 mm.

4.3 PERFORMANCE SUMMARIES

Results for the Open Field test broken out by size, depth and nonstandard ordnance are presented in Table 5 (for cost results, see section 5). Results by size and depth include both standard and nonstandard ordnance. The results by size show how well the demonstrator did at detecting/discriminating ordnance of a certain caliber range (see app A for size definitions). The results are relative to the number of ordnance items emplaced. Depth is measured from the geometric center of anomalies.

The RESPONSE STAGE results are derived from the list of anomalies above the demonstrator-provided noise level. The results for the DISCRIMINATION STAGE are derived from the demonstrator's recommended threshold for optimizing UXO field cleanup by minimizing false digs and maximizing ordnance recovery. The lower 90 percent confidence limit on probability of detection and P_{fp} was calculated assuming that the number of detections and false positives are binomially distributed random variables. All results in Table 5 have been rounded to protect the ground truth. However, lower confidence limits were calculated using actual results.

TABLE 5. SUMMARY OF OPEN FIELD RESULTS FOR GEM-5/TOWED ARRAY

			By Size			By Depth, m			
Metric	Overall	Standard	Nonstandard	Small	Medium	Large	< 0.3	0.3 to <1	>= 1
			RESPONSE S	STAGE					
P _d	0.60	0.65	0.45	0.60	0.60	0.60	0.70	0.55	0.35
P _d Low 90% Conf	0.55	0.61	0.39	0.53	0.53	0.51	0.63	0.50	0.26
P _d Upper 90% Conf	0.62	0.70	0.52	0.66	0.63	0.67	0.72	0.63	0.43
Pfp	0.50	12	-	-	7	-	0.50	0.50	0.30
P _{fp} Low 90% Conf	0.48		Y		L Y	-	0.47	0.48	0.16
P _{fp} Upper 90% Conf	0.53	н	-		-	-	0.53	0.54	0.50
P _{fp}	0.60	-		-		-	-	-	-
			DISCRIMINATION	ON STAG	E				
P _d	0.35	0.35	0.25	0.25	0.45	0.20	0.45	0.30	0.05
P _d Low 90% Conf	0.29	0.33	0.20	0.18	0.39	0.13	0.39	0.23	0.01
P _d Upper 90% Conf	0.36	0.41	0.31	0.30	0.49	0.26	0.49	0.36	0.09
Pfp	0.15	-			X	7	0.20	0.15	0.05
Pfp Low 90% Conf	0.15	-	-	1	7	-	0.17	0.12	0.01
P _{fp} Upper 90% Conf	0.18	-	-			-	0.21	0.17	0.22
Pfp	0.10	-	, ja		-		-	-	-

Response Stage Noise Level: 20.00

Recommended Discrimination Stage Threshold: 5.00

Note: The recommended discrimination stage threshold values are provided by the demonstrator.

4.4 EFFICIENCY, REJECTION RATES, AND TYPE CLASSIFICATION

Efficiency and rejection rates are calculated to quantify the discrimination ability at specific points of interest on the ROC curve: (1) at the point where no decrease in P_d is suffered (i.e., the efficiency is by definition equal to one) and (2) at the operator selected threshold. These values are reported in Table 6.

TABLE 6. EFFICIENCY AND REJECTION RATES

	Efficiency (E)	False Positive Rejection Rate	Background Alarm Rejection Rate
At Operating Point	0.56	0.67	0.82
With No Loss of Pd	1.00	0.00	0.00

At the demonstrator's recommended setting, the ordnance items that were detected and correctly discriminated were further scored on whether their correct type could be identified (table 7). Correct type examples include "20-mm projectile, 105-mm HEAT Projectile, and 2.75-inch Rocket". A list of the standard type declaration required for each ordnance item was provided to demonstrators prior to testing. For example, the standard type for the three example items are 20mmP, 105H, and 2.75in, respectively.

TABLE 7. CORRECT TYPE CLASSIFICATION
OF TARGETS CORRECTLY
DISCRIMINATED AS UXO

Percentage Correct		
84.0		
46.7		
50.0		
55.3		

4.5 LOCATION ACCURACY

The mean location error and standard deviations appear in Table 8. These calculations are based on average missed depth for ordnance correctly identified in the discrimination stage. Depths are measured from the closest point of the ordnance to the surface. For the Blind Grid, only depth errors are calculated, since (X, Y) positions are known to be the centers of each grid square.

TABLE 8. MEAN LOCATION ERROR AND STANDARD DEVIATION (M)

	Mean	Standard Deviation
Northing	0.04	0.15
Easting	0.00	0.17
Depth	0.10	0.19

SECTION 5. ON-SITE LABOR COSTS

A standardized estimate for labor costs associated with this effort was calculated as follows: the first person at the test site was designated "supervisor", the second person was designated "data analyst", and the third and following personnel were considered "field support". Standardized hourly labor rates were charged by title: supervisor at \$95.00/hour, data analyst at \$57.00/hour, and field support at \$28.50/hour.

Government representatives monitored on-site activity. All on-site activities were grouped into one of ten categories: initial setup/mobilization, daily setup/stop, calibration, collecting data, downtime due to break/lunch, downtime due to equipment failure, downtime due to equipment/data checks or maintenance, downtime due to weather, downtime due to demonstration site issue, or demobilization. See Appendix D for the daily activity log. See section 3.4 for a summary of field activities.

The standardized cost estimate associated with the labor needed to perform the field activities is presented in Table 9. Note that calibration time includes time spent in the Calibration Lanes as well as field calibrations. "Site survey time" includes daily setup/stop time, collecting data, breaks/lunch, downtime due to equipment/data checks or maintenance, downtime due to failure, and downtime due to weather.

TABLE 9. ON-SITE LABOR COSTS

	No. People	Hourly Wage	Hours	Cost
		Initial Setup		
Supervisor	1	\$95.00	13.5	\$1,282.50
Data Analyst	1	57.00	13.5	769.50
Field Support	0	28.50	13.5	0.00
SubTotal				\$2,052.00
		Calibration		
Supervisor	1	\$95.00	1.16	\$110.20
Data Analyst	1	57.00	1.16	66.12
Field Support	0	28.50	1.16	0.00
SubTotal				\$176.32
		Site Survey		
Supervisor	1	\$95.00	47.50	\$4,512.50
Data Analyst	1	57.00	47.50	2,707.50
Field Support	0	28.50	47.50	0.00
SubTotal				\$7,220.00

See notes at end of table.

TABLE 9 (CONT'D)

	No. People	Hourly Wage	Hours	Cost
]	Demobilization		
Supervisor	1	\$95.00	2.08	\$110.20
Data Analyst	1	57.00	2.08	66.12
Field Support	0	28.50	2.08	0.00
Subtotal				\$316.16
Total				\$9,764.48

Notes: Calibration time includes time spent in the Calibration Lanes as well as calibration before each data run.

Site Survey time includes daily setup/stop time, collecting data, breaks/lunch, downtime due to system maintenance, failure, and weather.

SECTION 6. COMPARISON OF RESULTS TO BLIND GRID DEMONSTRATION

6.1 SUMMARY OF RESULTS FROM BLIND GRID DEMONSTRATION

Table 10 shows the results from blind grid survey conducted prior to surveying the open field during the same site visit in October of 2005. For more details on the blind grid survey results reference section 2.1.6.

TABLE 10. SUMMARY OF BLIND GRID RESULTS FOR THE GEM-5/TOWED ARRAY

	Overall	Standard	Nonstandard	By Size			By Depth, m		
Metric				Small	Medium	Large	< 0.3	0.3 to <1	>= 1
			RESPONSE S	TAGE					
P _d	0.60	0.65	0.55	0.65	0.50	0.60	0.85	0.55	0.15
P _d Low 90% Conf	0.53	0.55	0.42	0.57	0.39	0.35	0.75	0.45	0.03
P _d Upper 90% Conf	0.68	0.74	0.66	0.77	0.64	0.81	0.93	0.69	0.30
P _{fp}	0.65	-	-	-	-	-	0.70	0.65	0.00
P _{fp} Low 90% Conf	0.56	-	-	-	-	-	0.58	0.56	0.00
P _{fp} Upper 90% Conf	0.70	-		-	-	-	0.78	0.75	0.32
P _{ba}	0.05	-		1-		-	-	1-	-
			DISCRIMINATIO	ON STAG	E	•			
P _d	0.35	0.45	0.20	0.25	0.40	0.50	0.40	0.40	0.05
P _d Low 90% Conf	0.27	0.34	0.11	0.15	0.31	0.27	0.29	0.29	0.01
P _d Upper 90% Conf	0.41	0.53	0.31	0.34	0.55	0.73	0.52	0.52	0.22
Pfp	0.40	-	-	-		-	0.35	0.50	0.00
P _{fp} Low 90% Conf	0.32	-		-	-	-	0.24	0.38	0.00
P _{fp} Upper 90% Conf	0.46	-	-	-		-	0.44	0.58	0.32
Pba	0.00	-	-	-	-	-	-	-	-

6.2 COMPARISON OF ROC CURVES USING ALL ORDNANCE CATEGORIES

Figure 6 shows P_d^{res} versus the respective P_{fp} over all ordnance categories. Figure 7 shows P_d^{disc} versus their respective P_{fp} over all ordnance categories. Figure 7 uses horizontal lines to illustrate the performance of the demonstrator at the recommended discrimination threshold levels, defining the subset of targets the demonstrator would recommend digging based on discrimination.

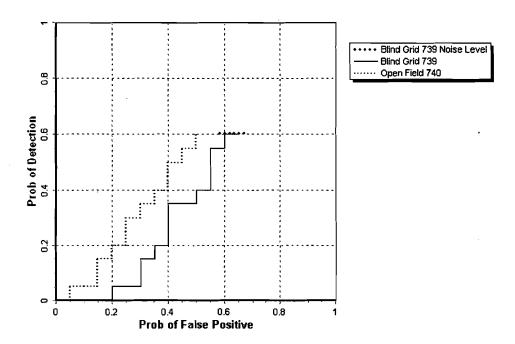


Figure 6. GEM-5/towed array P_d^{res} stages versus the respective P_{fp} over all ordnance categories combined.

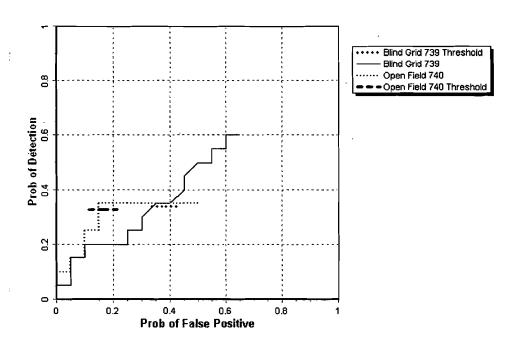


Figure 7. GEM-5/towed array $P_d^{\, disc}$ versus the respective P_{fp} over all ordnance categories combined.

6.3 COMPARISON OF ROC CURVES USING ORDNANCE LARGER THAN 20 MM

Figure 8 shows the P_d^{res} versus the respective probability of P_{fp} over ordnance larger than 20 mm. Figure 9 shows P_d^{disc} versus the respective P_{fp} over ordnance larger than 20 mm. Figure 9 uses horizontal lines to illustrate the performance of the demonstrator at the recommended discrimination threshold levels, defining the subset of targets the demonstrator would recommend digging based on discrimination.

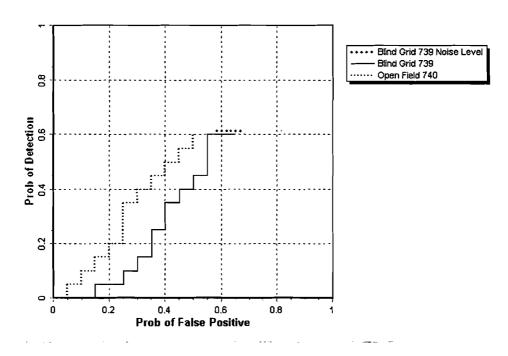


Figure 8. GEM-5/towed array P_d^{res} versus the respective P_{fp} for ordnance larger than 20 mm.

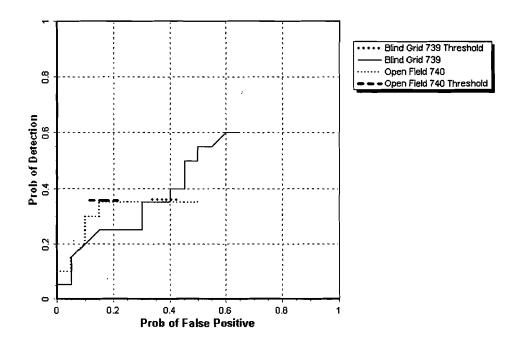


Figure 9. GEM-5/towed array P_d^{disc} versus the respective P_{fp} for ordnance larger than 20 mm.

6.4 STATISTICAL COMPARISONS

Statistical Chi-square significance tests were used to compare results between the Blind Grid and Open Field scenarios. The intent of the comparison is to determine if the feature introduced in each scenario has a degrading effect on the performance of the sensor system. However, any modifications in the UXO sensor system during the test, like changes in the processing or changes in the selection of the operating threshold, will also contribute to performance differences.

The Chi-square test for comparison between ratios was used at a significance level of 0.05 to compare Blind Grid to Open Field with regard to P_d^{res} , P_d^{disc} , P_{fp}^{res} and P_{fp}^{disc} , Efficiency and Rejection Rate. These results are presented in Table 11. A detailed explanation and example of the Chi-square application is located in Appendix A.

TABLE 11. CHI-SQUARE RESULTS - BLIND GRID VERSUS OPEN FIELD

Metric	Small	Medium	Large	Overall
P _d res	Not Significant	Not Significant	Not Significant	Not Significant
P _d disc	Not Significant	Not Significant	Significant	Not Significant
P _{fp} res	Not Significant	Not Significant	Not Significant	Not Significant
P _{fp} disc	-	-	-	Significant
Efficiency	•			Significant
Rejection rate	-	•	-	Significant

SECTION 7. APPENDIXES

APPENDIX A. TERMS AND DEFINITIONS

GENERAL DEFINITIONS

Anomaly: Location of a system response deemed to warrant further investigation by the demonstrator for consideration as an emplaced ordnance item.

Detection: An anomaly location that is within R_{halo} of an emplaced ordnance item.

Munitions and Explosives Of Concern (MEC): Specific categories of military munitions that may pose unique explosive safety risks, including UXO as defined in 10 USC 101(e)(5), DMM as defined in 10 USC 2710(e)(2) and/or munitions constituents (e.g. TNT, RDX) as defined in 10 USC 2710(e)(3) that are present in high enough concentrations to pose an explosive hazard.

Emplaced Ordnance: An ordnance item buried by the government at a specified location in the test site.

Emplaced Clutter: A clutter item (i.e., non-ordnance item) buried by the government at a specified location in the test site.

 R_{halo} : A pre-determined radius about the periphery of an emplaced item (clutter or ordnance) within which a location identified by the demonstrator as being of interest is considered to be a response from that item. If multiple declarations lie within R_{halo} of any item (clutter or ordnance), the declaration with the highest signal output within the R_{halo} will be utilized. For the purpose of this program, a circular halo 0.5 meters in radius will be placed around the center of the object for all clutter and ordnance items less than 0.6 meters in length. When ordnance items are longer than 0.6 meters, the halo becomes an ellipse where the minor axis remains 1 meter and the major axis is equal to the length of the ordnance plus 1 meter.

Small Ordnance: Caliber of ordnance less than or equal to 40 mm (includes 20-mm projectile, 40-mm projectile, submunitions BLU-26, BLU-63, and M42).

Medium Ordnance: Caliber of ordnance greater than 40 mm and less than or equal to 81 mm (includes 57-mm projectile, 60-mm mortar, 2.75 in. Rocket, MK118 Rockeye, 81-mm mortar).

Large Ordnance: Caliber of ordnance greater than 81 mm (includes 105-mm HEAT, 105-mm projectile, 155-mm projectile, 500-pound bomb).

Shallow: Items buried less than 0.3 meter below ground surface.

Medium: Items buried greater than or equal to 0.3 meter and less than 1 meter below ground surface.

Deep: Items buried greater than or equal to 1 meter below ground surface.

Response Stage Noise Level: The level that represents the point below which anomalies are not considered detectable. Demonstrators are required to provide the recommended noise level for the Blind Grid test area.

Discrimination Stage Threshold: The demonstrator selected threshold level that they believe provides optimum performance of the system by retaining all detectable ordnance and rejecting the maximum amount of clutter. This level defines the subset of anomalies the demonstrator would recommend digging based on discrimination.

Binomially Distributed Random Variable: A random variable of the type which has only two possible outcomes, say success and failure, is repeated for n independent trials with the probability p of success and the probability 1-p of failure being the same for each trial. The number of successes x observed in the n trials is an estimate of p and is considered to be a binomially distributed random variable.

RESPONSE AND DISCRIMINATION STAGE DATA

The scoring of the demonstrator's performance is conducted in two stages. These two stages are termed the RESPONSE STAGE and DISCRIMINATION STAGE. For both stages, the probability of detection (P_d) and the false alarms are reported as receiver operating characteristic (ROC) curves. False alarms are divided into those anomalies that correspond to emplaced clutter items, measuring the probability of false positive (P_{fp}) and those that do not correspond to any known item, termed background alarms.

The RESPONSE STAGE scoring evaluates the ability of the system to detect emplaced targets without regard to ability to discriminate ordnance from other anomalies. For the RESPONSE STAGE, the demonstrator provides the scoring committee with the location and signal strength of all anomalies that the demonstrator has deemed sufficient to warrant further investigation and/or processing as potential emplaced ordnance items. This list is generated with minimal processing (e.g., this list will include all signals above the system noise threshold). As such, it represents the most inclusive list of anomalies.

The DISCRIMINATION STAGE evaluates the demonstrator's ability to correctly identify ordnance as such, and to reject clutter. For the same locations as in the RESPONSE STAGE anomaly list, the DISCRIMINATION STAGE list contains the output of the algorithms applied in the discrimination-stage processing. This list is prioritized based on the demonstrator's determination that an anomaly location is likely to contain ordnance. Thus, higher output values are indicative of higher confidence that an ordnance item is present at the specified location. For electronic signal processing, priority ranking is based on algorithm output. For other systems, priority ranking is based on human judgment. The demonstrator also selects the threshold that the demonstrator believes will provide "optimum" system performance, (i.e., that retains all the detected ordnance and rejects the maximum amount of clutter).

Note: The two lists provided by the demonstrator contain identical numbers of potential target locations. They differ only in the priority ranking of the declarations.

RESPONSE STAGE DEFINITIONS

Response Stage Probability of Detection (P_d^{res}): $P_d^{res} = (No. of response-stage detections)/(No. of emplaced ordnance in the test site).$

Response Stage False Positive (fp^{res}): An anomaly location that is within R_{halo} of an emplaced clutter item.

Response Stage Probability of False Positive (P_{fp}^{res}): $P_{fp}^{res} = (No. of response-stage false positives)/(No. of emplaced clutter items).$

Response Stage Background Alarm (ba^{res}): An anomaly in a blind grid cell that contains neither emplaced ordnance nor an emplaced clutter item. An anomaly location in the open field or scenarios that is outside R_{halo} of any emplaced ordnance or emplaced clutter item.

Response Stage Probability of Background Alarm (P_{ba}^{res}): Blind Grid only: $P_{ba}^{res} = (No. of response-stage background alarms)/(No. of empty grid locations).$

Response Stage Background Alarm Rate (BAR^{res}): Open Field only: BAR^{res} = (No. of response-stage background alarms)/(arbitrary constant).

Note that the quantities P_d^{res} , P_{fp}^{res} , P_{ba}^{res} , and BAR^{res} are functions of t^{res} , the threshold applied to the response-stage signal strength. These quantities can therefore be written as $P_d^{res}(t^{res})$, $P_{fp}^{res}(t^{res})$, $P_{ba}^{res}(t^{res})$, and $P_d^{res}(t^{res})$.

DISCRIMINATION STAGE DEFINITIONS

Discrimination: The application of a signal processing algorithm or human judgment to response-stage data that discriminates ordnance from clutter. Discrimination should identify anomalies that the demonstrator has high confidence correspond to ordnance, as well as those that the demonstrator has high confidence correspond to nonordnance or background returns. The former should be ranked with highest priority and the latter with lowest.

Discrimination Stage Probability of Detection (P_d^{disc}) : $P_d^{disc} = (No. of discrimination-stage detections)/(No. of emplaced ordnance in the test site).$

Discrimination Stage False Positive (fp^{disc}): An anomaly location that is within R_{halo} of an emplaced clutter item.

Discrimination Stage Probability of False Positive (P_{fp}^{disc}): $P_{fp}^{disc} = (No. of discrimination stage false positives)/(No. of emplaced clutter items).$

Discrimination Stage Background Alarm (ba^{disc}): An anomaly in a blind grid cell that contains neither emplaced ordnance nor an emplaced clutter item. An anomaly location in the open field or scenarios that is outside R_{halo} of any emplaced ordnance or emplaced clutter item.

Discrimination Stage Probability of Background Alarm (P_{ba}^{disc}): $P_{ba}^{disc} = (No. of discrimination-stage background alarms)/(No. of empty grid locations).$

Discrimination Stage Background Alarm Rate (BAR^{disc}): BAR^{disc} = (No. of discrimination-stage background alarms)/(arbitrary constant).

Note that the quantities P_d^{disc} , P_{fp}^{disc} , P_{ba}^{disc} , and BAR^{disc} are functions of t^{disc} , the threshold applied to the discrimination-stage signal strength. These quantities can therefore be written as $P_d^{disc}(t^{disc})$, $P_{fp}^{disc}(t^{disc})$, $P_{ba}^{disc}(t^{disc})$, and $BAR^{disc}(t^{disc})$.

RECEIVER-OPERATING CHARACERISTIC (ROC) CURVES

ROC curves at both the response and discrimination stages can be constructed based on the above definitions. The ROC curves plot the relationship between P_d versus P_{fp} and P_d versus BAR or P_{ba} as the threshold applied to the signal strength is varied from its minimum (t_{min}) to its maximum (t_{max}) value. Figure A-1 shows how P_d versus P_{fp} and P_d versus BAR are combined into ROC curves. Note that the "res" and "disc" superscripts have been suppressed from all the variables for clarity.

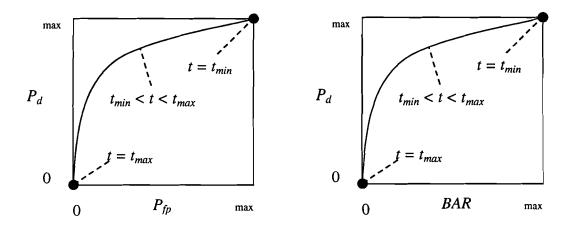


Figure A-1. ROC curves for open field testing. Each curve applies to both the response and discrimination stages.

¹Strictly speaking, ROC curves plot the P_d versus P_{ba} over a pre-determined and fixed number of detection opportunities (some of the opportunities are located over ordnance and others are located over clutter or blank spots). In an open field scenario, each system suppresses its signal strength reports until some bare-minimum signal response is received by the system. Consequently, the open field ROC curves do not have information from low signal-output locations, and, furthermore, different contractors report their signals over a different set of locations on the ground. These ROC curves are thus not true to the strict definition of ROC curves as defined in textbooks on detection theory. Note, however, that the ROC curves obtained in the Blind Grid test sites are true ROC curves.

METRICS TO CHARACTERIZE THE DISCRIMINATION STAGE

The demonstrator is also scored on efficiency and rejection ratio, which measure the effectiveness of the discrimination stage processing. The goal of discrimination is to retain the greatest number of ordnance detections from the anomaly list, while rejecting the maximum number of anomalies arising from nonordnance items. The efficiency measures the amount of detected ordnance retained by the discrimination, while the rejection ratio measures the fraction of false alarms rejected. Both measures are defined relative to the entire response list, i.e., the maximum ordnance detectable by the sensor and its accompanying false positive rate or background alarm rate.

Efficiency (E): $E = P_d^{disc}(t^{disc})/P_d^{res}(t_{min}^{res})$; Measures (at a threshold of interest), the degree to which the maximum theoretical detection performance of the sensor system (as determined by the response stage tmin) is preserved after application of discrimination techniques. Efficiency is a number between 0 and 1. An efficiency of 1 implies that all of the ordnance initially detected in the response stage was retained at the specified threshold in the discrimination stage, t^{disc} .

False Positive Rejection Rate (R_{fp}) : $R_{fp} = 1$ - $[P_{fp}^{disc}(t^{disc})/P_{fp}^{res}(t_{min}^{res})]$; Measures (at a threshold of interest), the degree to which the sensor system's false positive performance is improved over the maximum false positive performance (as determined by the response stage tmin). The rejection rate is a number between 0 and 1. A rejection rate of 1 implies that all emplaced clutter initially detected in the response stage were correctly rejected at the specified threshold in the discrimination stage.

Background Alarm Rejection Rate (Rba):

Blind Grid:
$$R_{ba} = 1 - [P_{ba}^{\ disc}(t^{disc})/P_{ba}^{\ res}(t_{min}^{\ res})].$$

Open Field: $R_{ba} = 1 - [BAR^{disc}(t^{disc})/BAR^{res}(t_{min}^{\ res})]).$

Measures the degree to which the discrimination stage correctly rejects background alarms initially detected in the response stage. The rejection rate is a number between 0 and 1. A rejection rate of 1 implies that all background alarms initially detected in the response stage were rejected at the specified threshold in the discrimination stage.

CHI-SQUARE COMPARISON EXPLANATION:

The Chi-square test for differences in probabilities (or 2 x 2 contingency table) is used to analyze two samples drawn from two different populations to see if both populations have the same or different proportions of elements in a certain category. More specifically, two random samples are drawn, one from each population, to test the null hypothesis that the probability of event A (some specified event) is the same for both populations (ref 3).

A 2 x 2 contingency table is used in the Standardized UXO Technology Demonstration Site Program to determine if there is reason to believe that the proportion of ordnance correctly detected/discriminated by demonstrator X's system is significantly degraded by the more challenging terrain feature introduced. The test statistic of the 2 x 2 contingency table is the

Chi-square distribution with one degree of freedom. Since an association between the more challenging terrain feature and relatively degraded performance is sought, a one-sided test is performed. A significance level of 0.05 is chosen which sets a critical decision limit of 2.71 from the Chi-square distribution with one degree of freedom. It is a critical decision limit because if the test statistic calculated from the data exceeds this value, the two proportions tested will be considered significantly different. If the test statistic calculated from the data is less than this value, the two proportions tested will be considered not significantly different.

An exception must be applied when either a 0 or 100 percent success rate occurs in the sample data. The Chi-square test cannot be used in these instances. Instead, Fischer's test is used and the critical decision limit for one-sided tests is the chosen significance level, which in this case is 0.05. With Fischer's test, if the test statistic is less than the critical value, the proportions are considered to be significantly different.

Standardized UXO Technology Demonstration Site examples, where blind grid results are compared to those from the open field and open field results are compared to those from one of the scenarios, follow. It should be noted that a significant result does not prove a cause and effect relationship exists between the two populations of interest; however, it does serve as a tool to indicate that one data set has experienced a degradation in system performance at a large enough level than can be accounted for merely by chance or random variation. Note also that a result that is not significant indicates that there is not enough evidence to declare that anything more than chance or random variation within the same population is at work between the two data sets being compared.

Demonstrator X achieves the following overall results after surveying each of the three progressively more difficult areas using the same system (results indicate the number of ordnance detected divided by the number of ordnance emplaced):

Blind Grid	Open Field	Moguls
$P_d^{res} 100/100 = 1.0$	8/10 = .80	20/33 = .61
$P_d^{disc} 80/100 = 0.80$	6/10 = .60	8/33 = .24

P_d^{res}: BLIND GRID versus OPEN FIELD. Using the example data above to compare probabilities of detection in the response stage, all 100 ordnance out of 100 emplaced ordnance items were detected in the blind grid while 8 ordnance out of 10 emplaced were detected in the open field. Fischer's test must be used since a 100 percent success rate occurs in the data. Fischer's test uses the four input values to calculate a test statistic of 0.0075 that is compared against the critical value of 0.05. Since the test statistic is less than the critical value, the smaller response stage detection rate (0.80) is considered to be significantly less at the 0.05 level of significance. While a significant result does not prove a cause and effect relationship exists between the change in survey area and degradation in performance, it does indicate that the detection ability of demonstrator X's system seems to have been degraded in the open field relative to results from the blind grid using the same system.

- P_d disc: BLIND GRID versus OPEN FIELD. Using the example data above to compare probabilities of detection in the discrimination stage, 80 out of 100 emplaced ordnance items were correctly discriminated as ordnance in blind grid testing while 6 ordnance out of 10 emplaced were correctly discriminated as such in open field-testing. Those four values are used to calculate a test statistic of 1.12. Since the test statistic is less than the critical value of 2.71, the two discrimination stage detection rates are considered to be not significantly different at the 0.05 level of significance.
- P_d^{res}: OPEN FIELD versus MOGULS. Using the example data above to compare probabilities of detection in the response stage, 8 out of 10 and 20 out of 33 are used to calculate a test statistic of 0.56. Since the test statistic is less than the critical value of 2.71, the two response stage detection rates are considered to be not significantly different at the 0.05 level of significance.
- P_d^{disc}: OPEN FIELD versus MOGULS. Using the example data above to compare probabilities of detection in the discrimination stage, 6 out of 10 and 8 out of 33 are used to calculate a test statistic of 2.98. Since the test statistic is greater than the critical value of 2.71, the smaller discrimination stage detection rate is considered to be significantly less at the 0.05 level of significance. While a significant result does not prove a cause and effect relationship exists between the change in survey area and degradation in performance, it does indicate that the ability of demonstrator X to correctly discriminate seems to have been degraded by the mogul terrain relative to results from the flat open field using the same system.

APPENDIX B. DAILY WEATHER LOGS

Date & Time	Average Temperature, °F	Total Precipitation, in.
10/05/2005 0700	62.9	0.00
10/05/2005 0800	64.5	0.00
10/05/2005 0900	65.8	0.00
10/05/2005 1000	67.3	0.00
10/05/2005 1100	68.1	0.00
10/05/2005 1200	68.5	0.00
10/05/2005 1300	70.6	0.00
10/05/2005 1400	73.2	0.00
10/05/2005 1500	75.7	0.00
10/05/2005 1600	77.2	0.00
10/05/2005 1700	78.1	0.00
10/06/2005 0700	66.5	0.00
10/06/2005 0800	66.9	0.00
10/06/2005 0900	68.1	0.00
10/06/2005 1000	69.0	0.00
10/06/2005 1100	69.7	0.00
10/06/2005 1200	70.3	0.00
10/06/2005 1300	72.8	0.00
10/06/2005 1400	74.7	0.00
10/06/2005 1500	76.7	0.00
10/06/2005 1600	77.5	0.00
10/06/2005 1700	74.9	0.06
10/07/2005 0700	71.9	0.00
10/07/2005 0800	72.2	0.00
10/07/2005 0900	73.3	0.00
10/07/2005 1000	74.2	0.00
10/07/2005 1100	74.7	0.01
10/07/2005 1200	75.8	0.00
10/07/2005 1300	77.4	0.00
10/07/2005 1400	77.9	0.01
10/07/2005 1500	76.3	0.05
10/07/2005 1600	76.3	0.13
10/07/2005 1700	76.0	0.01

Date & Time	Average Temperature, °F	Total Precipitation, in.
10/17/2005 0700	46.9	0.00
10/17/2005 0800	47.2	0.00
10/17/2005 0900	52.9	0.00
10/17/2005 1000	57.2	0.00
10/17/2005 1100	59.7	0.00
10/17/2005 1200	61.6	0.00
10/17/2005 1300	63.3	0.00
10/17/2005 1400	64.6	0.00
10/17/2005 1500	65.3	0.00
10/17/2005 1600	66.2	0.00
10/17/2005 1700	66.7	0.00
10/18/2005 0700	50.6	0.00
10/18/2005 0800	54.0	0.00
10/18/2005 0900	55.9	0.00
10/18/2005 1000	59.7	0.00
10/18/2005 1100	67.2	0.00
10/18/2005 1200	72.5	0.00
10/18/2005 13:00	74.3	0.00
10/18/2005 1400	75.5	0.00
10/18/2005 1500	75.5	0.00
10/18/2005 1600	76.5	0.00
10/18/2005 1700	76.8	0.00
10/19/2005 0700	44.2	0.00
10/19/2005 0800	43.6	0.00
10/19/2005 0900	50.2	0.00
10/19/2005 1000	58.0	0.00
10/19/2005 1100	63.3	0.00
10/19/2005 1200	66.8	0.00
10/19/2005 1300	68.5	0.00
10/19/2005 1400	69.9	0.00
10/19/2005 1500	70.9	0.00
10/19/2005 1600	71.9	0.00
10/19/2005 1700	71.7	0.00
10/20/2005 0700	58.2	0.00
10/20/2005 0800	56.6	0.00
10/20/2005 0900	55.7	0.00
10/20/2005 1000	54.3	0.00
10/20/2005 1100	53.9	0.00
10/20/2005 1200	54.4	0.00
10/20/2005 1300	54.5	0.00
10/20/2005 1400	55.2	0.00
10/20/2005 1500	55.3	0.00
10/20/2005 1600	54.6	0.00
10/20/2005 1700	53.2	0.00

Date & Time	Average Temperature, °F	Total Precipitation, in.
10/21/2005 0700	54.1	0.00
10/21/2005 0800	53.1	0.01
10/21/2005 0900	49.9	0.03
10/21/2005 1000	49.7	0.04
10/21/2005 1100	49.9	0.03
10/21/2005 1200	50.7	0.03
10/21/2005 1300	51.2	0.01
10/21/2005 1400	51.5	0.00
10/21/2005 1500	51.6	0.00
10/21/2005 1600	51.4	0.00
10/21/2005 1700	51.3	0.00

APPENDIX C. SOIL MOISTURE

Date: 10/05/2005

Times: 1100 through 1600

Probe Location	Layer, in.	AM Reading, %	PM Reading, %
	0 to 6	NA	NA
•	6 to 12	NA	NA
Wet Area	12 to 24	NA	NA
	24 to 36	NA	NA
	36 to 48	NA	NA
	0 to 6		NA NA
	6 to 12	NA	NA NA
Wooded Area	12 to 24	NA	NA NA
	24 to 36	NA	NA NA
	36 to 48	NA	NA
	0 to 6		NA NA
	6 to 12	NA NA	NA
Open Area	12 to 24	NA	NA
·	24 to 36	NA NA	NA
<u> </u>	36 to 48	NA	NA
	1 04.6		1 04
	0 to 6	0.4	0.4
	6 to 12	14.1	14.0
Calibration Lanes	12 to 24	22.1	21.8
	24 to 36	26.4	26.3
	36 to 48	27.2	27.0
	0 to 6	2.0	2.0
	6 to 12	4.2	4.1
Blind Grid/Moguls	12 to 24	22.3	22.4
J	24 to 36	3.1	3.0
	36 to 48	2.3	2.4

Date: 10/06/2005

Probe Location	Layer, in.	AM Reading, %	PM Reading, %
	0 to 6	NA	NA
	6 to 12	NA	NA
Wet Area	12 to 24	NA	NA
	24 to 36	NA	NA
	36 to 48	NA	NA
	0 to 6	NA	NA
	6 to 12	NA NA	NA
Wooded Area	12 to 24	NA	NA NA
	24 to 36	NA	NA
	36 to 48	NA	NA
	<u> </u>	<u> </u>	
	0 to 6	NA	NA
	6 to 12	NA	NA
Open Area	12 to 24	NA	NA
	24 to 36	NA	NA
·	36 to 48	NA	NA
	_		
	0 to 6	0.3	0.3
	6 to 12	13.9	14.2
Calibration Lanes	12 to 24	21.4	21.2
	24 to 36	26.4	26.0
	36 to 48	27.2	27.2
	0 to 6	1.9	1.9
	6 to 12	4.0	4.0
Blind Grid/Moguls	12 to 24	22.2	22.1
	24 to 36	2.8	2.8
	36 to 48	2.2	2.2

Date: 10/07/2005

Probe Location	Layer, in.	AM Reading, %	PM Reading, %
	0 to 6	2.3	2.3
	6 to 12	4.0	3.9
Wet Area	12 to 24	8.0	7.8
	24 to 36	2.2	2.1
	36 to 48	2.3	2.4
	0 to 6	NA	NA
	6 to 12	NA	NA
Wooded Area	12 to 24	NA	NA
	24 to 36	NA	NA
	36 to 48	NA	NA
	0 to 6	2.7	2.7
	6 to 12	3.0	2.9
Open Area	12 to 24	2.0	2.1
орен тиси	24 to 36	6.4	6.2
	36 to 48	11.2	11.3
	0 to 6	NA	NA
	6 to 12	NA	NA
Calibration Lanes	12 to 24	NA	NA
	24 to 36	NA	NA
	36 to 48	NA	NA
	0 to 6	NA	NA NA
	6 to 12	NA NA	NA
Blind Grid/Moguls	12 to 24	NA	NA NA
	24 to 36	NA	NA
	36 to 48	NA NA	NA

Date: 10/17/2005

Probe Location	Layer, in.	AM Reading, %	PM Reading, %
	0 to 6	4.7	4.8
	6 to 12	7.9	8.0
Wet Area	12 to 24	16.1	16.0
	24 to 36	4.5	4.4
	36 to 48	4.6	4.2
	0 to 6		NA
	6 to 12	NA NA	NA NA
Wooded Area	12 to 24	NA NA	NA NA
Wooded Tarea	24 to 36	NA NA	NA NA
	36 to 48	NA	NA
<u> </u>	0 to 6	5.4	5.3
	6 to 12	6.0	6.1
Open Area	12 to 24	4.1	4.0
Open raeu	24 to 36	12.8	12.7
	36 to 48	22.4	22.1
	0 to 6	NA	NA
	6 to 12	NA	NA
Calibration Lanes	12 to 24	NA	NA
	24 to 36	NA	NA
	36 to 48	NA	NA
	0 to 6		NA NA
	6 to 12	NA	NA
Blind Grid/Moguls	12 to 24	NA NA	NA
.	24 to 36	NA	NA
	36 to 48	NA	NA

Date: 10/18/2005

Probe Location	Layer, in.	AM Reading, %	PM Reading, %
	0 to 6	4.5	4.4
	6 to 12	7.9	8.1
Wet Area	12 to 24	16.0	15.9
	24 to 36	4.4	4.3
1.7	36 to 48	4.5	4.2
-	0 to 6	NA	NA
	6 to 12	NA	NA
Wooded Area	12 to 24	NA	NA
	24 to 36	NA	NA
	36 to 48	NA	NA
	0 to 6	5.5	5.6
	6 to 12	6.0	6.2
Open Area	12 to 24	4.0	3.8
	24 to 36	12.5	12.9
	36 to 48	22.3	22.0
	0 to 6	NA	NA
	6 to 12	NA	NA
Calibration Lanes	12 to 24	NA	NA
	24 to 36	NA	NA
	36 to 48	NA	NA
	0 to 6	NA	NA
	6 to 12	NA	NA
Blind Grid/Moguls	12 to 24	NA	NA
	24 to 36	NA	NA
	36 to 48	NA	NA

Date: 10/19/2005

Layer, in.	AM Reading, %	PM Reading, %
0 to 6	4.2	4.1
6 to 12	8.0	8.2
12 to 24	16.0	15.7
24 to 36	4.1	4.0
36 to 48	4.3	4.4
0 to 6	NA NA	NA
		NA NA
		NA NA
		NA
36 to 48	NA	. NA
0 to 6	53	5.5
		6.6
		3.6
		12.7
36 to 48	22.5	22.6
0 to 6	<u>NA</u>	NA
6 to 12	NA	NA
12 to 24	NA	NA
24 to 36	NA	NA
36 to 48	NA	NA
1 0 to 6	NA	NA NA
		NA NA
-		NA NA
		NA NA
36 to 48	NA NA	NA NA
	0 to 6 6 to 12 12 to 24 24 to 36 36 to 48 0 to 6 6 to 12 12 to 24 24 to 36 36 to 48 0 to 6 6 to 12 12 to 24 24 to 36 36 to 48 0 to 6 6 to 12 12 to 24 24 to 36 36 to 48 0 to 6 6 to 12 12 to 24 24 to 36 36 to 48	0 to 6 4.2 6 to 12 8.0 12 to 24 16.0 24 to 36 4.1 36 to 48 4.3 0 to 6 NA 6 to 12 NA 12 to 24 NA 24 to 36 NA 36 to 48 NA 0 to 6 5.3 6 to 12 6.2 12 to 24 3.9 24 to 36 12.3 36 to 48 22.5 0 to 6 NA 6 to 12 NA 12 to 24 NA 24 to 36 NA 36 to 48 NA

Date: 10/20/2005

Probe Location	Layer, in.	AM Reading, %	PM Reading, %
	0 to 6	4.4	4.7
	6 to 12	8.6	8.5
Wet Area	12 to 24	16.0	16.5
	24 to 36	4.5	4.7
	36 to 48	4.5	4.9
	0 to 6	NA	NA
	6 to 12	NA	NA
Wooded Area	12 to 24	NA	NA
	24 to 36	NA	NA
	36 to 48	NA	NA
	0 to 6	5.2	5.7
0 4	6 to 12	6.5	
Open Area	12 to 24	3.8	4.6
	24 to 36	12.2	12.9
	36 to 48	22.9	23.5
	0 to 6	NA	NA
	6 to 12	NA NA	NA NA
Calibration Lanes	12 to 24	NA NA	NA NA
	24 to 36	NA	NA
	36 to 48	NA	NA
	•		
	0 to 6	NA	NA
	6 to 12	NA	NA
Blind Grid/Moguls	12 to 24	NA	NA
	24 to 36	NA	ŅA
	36 to 48	NA	NA

Date: 10/21/2005

Probe Location	Layer, in.	AM Reading, %	PM Reading, %
	0 to 6	5.6	5.8
	6 to 12	9.5	9.9
Wet Area	12 to 24	16.8	16.9
	24 to 36	5.8	5.9
_	36 to 48	5.9	6.2
	0 to 6	NA	NA
	6 to 12	NA	NA
Wooded Area	12 to 24	NA	NA
	24 to 36	NA	NA
	36 to 48	NA	NA
<u> </u>			,
	0 to 6	5.9	6.3
	6 to 12	7.5	7.8
Open Area	12 to 24	4.8	4.8
	24 to 36	13.8	13.8
- -	36 to 48	23.8	24.2
		<u> </u>	_
	0 to 6	NA	NA
	6 to 12	NA	NA
Calibration Lanes	12 to 24	NA	NA
	24 to 36	NA	NA NA
	36 to 48	NA	NA
			
	0 to 6	NA NA	NA NA
DU 101101	6 to 12	NA	NA
Blind Grid/Moguls	12 to 24	<u>NA</u>	NA
	24 to 36	NA	NA NA
	36 to 48	NA	NA

APPENDIX D. DAILY ACTIVITY LOG

			Statue	Status					Track		
	No. of		Start	Stop	Duration		Operational Status	Track	Method=Other		
Date	People	Area-Tested	Time	Time	min.	Operational Status	- Comments	Method	Explain	Pattern	Field Conditions
1000000	,	CALIBRATION	0301	000	0,7	of words as included		940		4.	
10/02/2002	7	LAINES	ncni	1330	001	INITIAL SETUR		SPS	AN	LINEAR	SUNNY, DRY
		CALIBRATION	140000000000000000000000000000000000000						0 70 00		
10/05/2005	2	LANES	1510	1545	35	INITIAL SETUP		CPS	NA A	LINEAR	SUNNY, DRY
10/06/2005	2	CALIBRATION LANES	740	1755	615	INITIAL SETTIP		SdD	Z	LINEAR	RAIN WET
		BLIND TEST				COLLECTING			1000		
10/06/2005	2	GRID	1755	1830	35	DATA		GPS	NA	LINEAR	RAIN, WET
		BLIND TEST				DAILY START,	EQUIPMENT				
10/06/2005	2	GRID	1830	1905	35	STOP	BREAKDOWN	CPS	NA	LINEAR	RAIN, WET
							DAILY				
						DAILY START,	EQUIPMENT			Short Control Control	
10/07/2005	2	OPEN FIELD	730	815	45	STOP	SETUP	GPS	NA	LINEAR	RAIN, WET
						COLLECTING					
10/07/2005	2	OPEN FIELD	815	1135	200	DATA		GPS	NA	LINEAR	RAIN, WET
10/07/2005	2	OPEN FIELD	1135	1150	15	BREAK/LUNCH		GPS	NA	LINEAR	RAIN, WET
						COLLECTING					
10/07/2005	2	OPEN FIELD	1150	1340	110	DATA		GPS	NA	LINEAR	RAIN, WET
						DAILY START,	EQUIPMENT				
10/07/2005	2	OPEN FIELD	1340	1400	20	STOP	BREAKDOWN	GPS	NA	LINEAR	RAIN, WET
						DOWNTIME DUE					
						TO EQUIP	DOWNLOAD				
10/07/2005	2	OPEN FIELD	1400	1415	15	MAINT/CHECK	DATA	GPS	NA	LINEAR	RAIN, WET
						DAILY START,	EQUIPMENT				
10/07/2005	7	OPEN FIELD	1415	1430	15	STOP	BREAKDOWN	GPS	NA	LINEAR	RAIN, WET
							DAILY				
The second second second second	8		-	The state of the s	The same of the sa	DAILY START,	EQUIPMENT			Section of the sectio	
10/17/2005	2	OPEN FIELD	740	855	75	STOP	SETUP	GPS	NA	LINEAR	SUNNY, DRY
		a sum summer			00.	COLLECTING		040			The state of the s
10/17/2005	7	OPEN FIELD	833	1702	061	DAIA		35	NA	LINEAR	SUNNY, DRY

Note: Activities pertinent to this specific demonstration are indicated in highlighted text.

		Status	Status					Track		
No. of		Start	Stop	Duration		Operational Status	Track	Method=Other		
People	Area-Tested	Time	Time	min.	Operational Status	· Comments	Method	Explain	Pattern	Field Conditions
	OPEN FIELD	1205	1245	40	BREAK/LUNCH		GPS	NA	LINEAR	SUNNY, DRY
	OPEN FIELD	1245	1655	250	COLLECTING		GPS	NA	LINEAR	SUNNY, DRY
						PVC JOINT SNAPPED CONNECTION TO				
					DOWNTIME DUE TO EQUIPMENT	NAVIGATION COMPUTER,				
	OPEN FIELD	1655	1800	65	FAILURE	FIXING	GPS	N. A.Z.	LINEAR	SUNNY, DRY
	OPEN FIELD	1800	1815	15	DAILY START, STOP	EQUIPMENT BREAKDOWN	GPS	NA	LINEAR	SUNNY, DRY
						PVC JOINT SNAPPED				
						CONNECTION TO				
					TO FOUR MENT	COMPLITER				
	OPEN FIELD	740	1220	280	FAILURE	FIXING	GPS	NA	LINEAR	SUNNY, DRY
ı					COLLECTING					
_	OPEN FIELD	1220	1710	290	DATA		GPS	NA	LINEAR	SUNNY, DRY
	ODEN FIELD	0121	1755	76	DAILY START,	EQUIPMENT	ODO	NIA	TATEAD	CIRRI DEV
1	Com I No Io	01/1	2011	2	TO IS	DAILY	2 5	ON	LUNEON	SOMMI, DAI
			1	İ	DAILY START,	EQUIPMENT SET				
	OPEN FIELD	725	845	80	STOP	UP	GPS	NA	LINEAR	SUNNY, DRY
	OPEN FIELD	845	1530	405	COLLECTING		GPS	NA	LINEAR	SUNNY, DRY
	A VIIII VALIDO	0000	0000	C	DAILY START,	EQUIPMENT	040			
- 1	OPEN FIELD	1530	0001	80	STOP	BREAKDOWN	SAS	AN	LINEAR	SUNNY, DKY
	OPEN FIELD	725	815	20	DAILY START, STOP	DAILY EQUIPMENT SETUP	Sdb	A'Z	LINEAR	CLOUDY,
•					· > · >		2	****		7000

Note: Activities pertinent to this specific demonstration are indicated in highlighted text.

			Status	Status					Track		ı
	No. of		Start	Stop	Duration		Operational Status	Track	Method=Other		
Date	People	Area-Tested	Time	Time	min.	Operational Status	- Comments	Method	Explain	Pattern	Field Conditions
			200			COLLECTING					CLOUDY,
10/20/2005	2	ACTIVE SITE	815	845	30	DATA		GPS	NA	LINEAR	T000
						COLLECTING					CLOUDY,
10/20/2005	2	OPEN FIELD	845	1015	90	DATA		GPS	NA	LINEAR	COOL
						DOWNTIME DUE					
	ļ					TO EQUIPMENT	PVC JOINT				CLOUDY,
10/20/2005	2	OPEN FIELD	1015	1405	230	FAILURE	SNAPPED, GLUED	GPS	NA	LINEAR	COOL
						COLLECTING					CLOUDY,
10/20/2005	2	OPEN FIELD	1405	1525	80	DATA		GPS	NA	LINEAR	COOL
						DOWNTIME DUE					
	1					TO EQUIPMENT	PVC JOINT				CLOUDY,
10/20/2005	2	OPEN FIELD	1525	1715	110	FAILURE	SNAPPED, GLUED	GPS	NA	LINEAR	COOL
						DAILY START,	EQUIPMENT				CLOUDY,
10/20/2005	2	OPEN FIELD	1715	1810	55	STOP	BREAKDOWN	GPS	NA	LINEAR	T000
						DAILY START,					
10/21/2005	2	ACTIVE SITE	650	755	65	STOP		GPS	NA	LINEAR	RAIN, WET
						COLLECTING					
10/21/2005	2	ACTIVE SITE	755	850	55	DATA		GPS	NA	LINEAR	RAIN, WET
							COULD NOT				
						DEMONISTE ATION	IN ABEA DITE TO				
10/21/2005	2	ACTIVE SITE	850	1115	145	SITE ISSUE	FIRING AT B1	CPS	Z	LINEAR	RAIN WET
						COLLECTING					
10/21/2005	2	ACTIVE SITE	1115	1240	85	DATA		GPS	NA	LINEAR	RAIN, WET
10/21/2005	2	OPEN FIELD	1240	1445	125	DEMOBILIZATION		GPS	NA	LINEAR	RAIN, WET
										The second secon	COLUMN ASSESSED.

Note: Activities pertinent to this specific demonstration are indicated in highlighted text.

APPENDIX E. REFERENCES

- 1. Standardized UXO Technology Demonstration Site Handbook, DTC Project No. 8-CO-160-000-473, Report No. ATC-8349, March 2002.
- 2. Aberdeen Proving Ground Soil Survey Report, October 1998.
- 3. Data Summary, UXO Standardized Test Site: APG Soils Description, May 2002.
- 4. Yuma Proving Ground Soil Survey Report, May 2003.

APPENDIX F. ABBREVIATIONS

ADC = analog-to-digital converters

AEC = U.S. Army Environmental Center

APG = Aberdeen Proving Ground

ATC = U.S. Army Aberdeen Test Center

DSP = digital signal processors EMI = electromagnetic interference

EMF = electromagnetic field

ERDC = U.S. Army Corps of Engineers Engineering Research and Development Center

ESTCP = Environmental Security Technology Certification Program

EQT = Army Environmental Quality Technology Program

GPS = Global Positioning System
JPG = Jefferson Proving Ground

POC = point of contact ppm = parts per million QA = quality assurance QC = quality control

ROC = receiver-operating characteristic

Rx = receiver coil

SERDP = Strategic Environmental Research and Development Program

Tx = transmitting coil

UTM = Universal Transverse Mercator

UXO = unexploded ordnance

YPG = U.S. Army Yuma Proving Ground

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